

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
20 February 2003 (20.02.2003)

PCT

(10) International Publication Number  
**WO 03/014263 A1**

(51) International Patent Classification<sup>7</sup>: **C10G 9/20**,  
B01J 19/02, C23C 30/00, C22C 9/00

(21) International Application Number: PCT/US02/23325

(22) International Filing Date: 19 July 2002 (19.07.2002)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
09/922,331 3 August 2001 (03.08.2001) US

(71) Applicant: **EXXONMOBIL RESEARCH AND ENGINEERING COMPANY** [US/US]; 1545 Route 22 East, P.O. Box 900, Annandale, NJ 08801-0900 (US).

(72) Inventors: **RAMANARAYANAN, Trikur, A.**; 16 Maher Road, Somerset, NJ 08873 (US). **CHUN, ChangMin**; 8112 Town Court North, Lawrenceville, NJ 08648 (US). **MUMFORD, James, D., III**; 334 Fairmount Road, Long Valley, NJ 07853 (US).

(74) Agents: **BAKUN, Estelle, C. et al.**; ExxonMobil Research and Engineering Company, 1545 Route 22 East, P.O. Box 900, Annandale, NJ 08801-0900 (US).

(81) Designated States (*national*): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA, ZM, ZW.

(84) Designated States (*regional*): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

**Published:**

— with international search report

*For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.*



**WO 03/014263 A1**

(54) Title: METAL DUSTING RESISTANT COPPER BASED ALLOY SURFACES

(57) Abstract: A method for inhibiting metal dusting corrosion of surfaces exposed to supersaturated carbon environments comprising constructing said surfaces of, or coating said surfaces with a copper based alloy. The invention is also directed to a composition resistant to metal dusting.

## METAL DUSTING RESISTANT COPPER BASED ALLOY SURFACES

### FIELD OF THE INVENTION

[0001] The invention herein described, includes alloys which are resistant to metal dusting.

### BACKGROUND OF THE INVENTION

[0002] High temperature alloys which are Fe, Ni, or Co based are prone to a virulent form of corrosion known as metal dusting when subjected to environments which are supersaturated with carbon. The problem is generally encountered at temperatures ranging from 300–850°C. Many processes of interest to the petrochemical industry which involve carbon-supersaturated environments, are limited by the lack of available reactor materials and heat exchanger materials that are resistant to metal dusting. Research has led to some understanding of the underlying mechanisms. For the Fe-based systems, the mechanism involves the initial formation of a metastable  $\text{Fe}_3\text{C}$  carbide on the alloy surface in the carbon-supersaturated environments. Subsequently, graphite deposits on the metastable carbide whereby it is destabilized and decomposes to iron particles and carbon, thus triggering the corrosion process. For Ni based and Co based systems, while no metastable surface carbide forms, graphite deposition on the metal provides channels through which the metal can migrate out. In addition, carbon also supersaturates the metal and causes profuse graphite precipitation in the interior, thus leading to a breaking up of the bulk metal.

[0003] The carbon-supersaturated environment that is encountered in process streams consists of either hydrocarbon molecules or carbon monoxide. Of these, the latter is a more virulent metal dusting molecule. Heyse and coworkers have proposed carburization and metal dusting resistant coating systems that are applicable to hydroalkylation processes where hydrocarbon is the main corrosive medium. The general approach to control metal dusting is the use of alloys that can form protective surface oxide films in the environment involved. But in most currently available alloy systems, the break up of the protective surface oxide film leads to local metal dusting corrosion.

[0004] Current approaches to control metal dusting involve the use of H<sub>2</sub>S as a gas phase corrosion inhibitor, expensive high temperature alloys and tin based coatings for selected applications involving hydrocarbon corrosives (See for example, Heyse, et.al. U.S. 5,863,418). However, even the more expensive alloys are not fully metal dusting resistant. Coating systems, especially based on tin, have limited applications in predominantly hydrocarbon environments. The use of H<sub>2</sub>S necessitates clean up of the downstream process gas. Further, in many catalytic processes, H<sub>2</sub>S can be a catalyst poison. Thus, its use is rather limited.

[0005] Certain coating materials have been taught in the prior art. For example, see U.S. 5,575,902 which teaches the use of Group VIB metals, specifically chromium for coating surfaces susceptible to carburization.

[0006] What is needed in the art are materials that are highly resistant to metal dusting corrosion in petrochemical processes where supersaturated carbon environments are present.

## BRIEF DESCRIPTION OF THE FIGURES

[0007] Figure 1 depicts the metal dusting rate (mpy) of Fe-1.25 Cr-0.5 Mo alloy as a function of CO-H<sub>2</sub> gas mixture at 538°C (1000°F). The hollow circles are the local rate and the solid circles are the general rate.

[0008] Figure 2 depicts the mass gain due to carbon deposition (a measure of metal dusting corrosion) of Cu-xSn alloys as a function of Sn content at 500°C in 50 CO:50 H<sub>2</sub> gas mixture after 65 hours of corrosion.

[0009] Figure 3 depicts the concentration profile of Sn in Cu-5Sn alloy as a function of distance from the surface after corrosion in 50 CO:50 H<sub>2</sub> gas mixture at 500°C after 65 hours.

[0010] Figure 4 depicts the concentration profile of Sn in Cu-8Sn alloy as a function of distance from the surface after corrosion in 50 CO:50 H<sub>2</sub> gas mixture

(a) at 650°C for 160 hours

(b) at 500°C for 66 hours

(c) at 400°C for 94 hours

[0011] Figure 5 depicts the mass gain due to carbon deposition of Cu-xGa alloy as a function of Ga content at 500°C in 50 CO:50 H<sub>2</sub> gas mixture after 65 hours of corrosion.

[0012] Figure 6 depicts the concentration profile of Ga in Cu-5Ga, Cu-2Ga, and Cu-1Ga alloys as a function of distance from the surface after corrosion in 50 CO:50 H<sub>2</sub> gas mixture at 500°C after 65 hours.

[0013] Figure 7 depicts the mass gain due to carbon deposition of Cu-xAl alloy as a function of Al content at 500 °C in 50 CO:50 H<sub>2</sub> gas mixture after 65 hour of corrosion at 500°C.

## SUMMARY OF THE INVENTION

[0014] An aspect of the invention comprises a composition resistant to metal dusting when exposed to a carbon super-saturated environment at temperatures up to about 650°C comprising an alloy selected from the group consisting of copper-tin alloys, copper-gallium alloys copper-aluminum alloys, and mixtures thereof, wherein when said alloy is a copper-tin alloy, the amount of tin will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures of about 400 to about 500°C, and about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 400°C, and wherein when said alloy is a copper-gallium alloy, the amount of gallium will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 up to about 650°C, and from about 0.1 to about 5 wt% for temperatures up to about 500° C, and wherein when said alloy is an copper-aluminum alloy, the amount of aluminum will range from about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and wherein when said mixture is a copper-tin-gallium alloy, the

amount of tin and gallium combined will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt % when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-tin-aluminum alloy , the amount of aluminum will be about 0.1 to about 8 wt% and the amount of tin will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of aluminum will be about 0.1 to about 4 wt% and the amount of tin will be about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-gallium-aluminum alloy the amount of gallium will be about 0.1 to about 5 wt% and the amount of aluminum will be about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of gallium will be about 0.1 to about 2 wt% and the amount of aluminum will be about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, and wherein when said mixture is a copper-tin-gallium-aluminum alloy, said alloy will contain about 0.1 to about 5 wt% of gallium and tin combined and about 0.1 to about 8 wt% aluminum when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt% of gallium and tin combined and about 0.1 to about 4 wt% aluminum when exposed to carbon supersaturated environments of between about 500 and about 650°C.

[0015] Another aspect of the invention is directed to a method for inhibiting metal dusting of surfaces exposed to supersaturated carbon environments comprising constructing said surfaces of, or coating said surfaces with an alloy selected from the group consisting of copper-tin alloys, copper-gallium alloys copper-aluminum alloys, and mixtures thereof, wherein when said

alloy is a copper-tin alloy, the amount of tin will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures of about 400 to about 500°C, and about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 400°C, and wherein when said alloy is a copper-gallium alloy, the amount of gallium will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 up to about 650°C, and from about 0.1 to about 5 wt% for temperatures up to about 500°C, and wherein when said alloy is an copper-aluminum alloy, the amount of aluminum will range from about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and wherein when said mixture is a copper-tin-gallium alloy, the amount of tin and gallium combined will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt % when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-tin-aluminum alloy, the amount of aluminum will be about 0.1 to about 8 wt% and the amount of tin will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of aluminum will be about 0.1 to about 4 wt% and the amount of tin will be about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-gallium-aluminum alloy the amount of gallium will be about 0.1 to about 5 wt% and the amount of aluminum will be about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of gallium will be about 0.1 to about 2 wt% and the amount of aluminum will be

about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, and wherein when said mixture is a copper-tin-gallium-aluminum alloy, said alloy will contain about 0.1 to about 5 wt% of gallium and tin combined and about 0.1 to about 8 wt% aluminum when exposed to carbon supersaturated environments at temperatures up to about 500 °C and about 0.1 to about 2 wt% of gallium and tin combined and about 0.1 to about 4 wt% aluminum when exposed to carbon supersaturated environments of between about 500 and about 650°C.

[0016] A carbon super-saturated environment is herein defined as an environment where the thermodynamic activity of carbon is greater than unity.

#### DETAILED DESCRIPTION

[0017] In many high temperature (300 to 850°C) hydrocarbon-processing applications, structural components such as reactors and heat exchangers can be degraded by a carbon-induced corrosion known as metal dusting. Since the rate of such corrosion can sometimes exceed ~ 25 millimeters per year (1000 mils per year), controlling it is important for both economic and safety reasons.

[0018] One aspect of the invention herein described uses a metal that suppresses graphite deposition, which is an essential step in metal dusting corrosion, and thereby controls metal dusting. For practical use such a metal must be economically attractive and reasonably high melting. In the present invention, copper and copper-based alloys are utilized as the surface contacting the carbon super-saturated environment which causes metal dusting corrosion.

[0019] The invention is specifically applicable, but not limited, to process streams where CO – H<sub>2</sub> mixtures constitute the predominant metal dusting medium.

[0020] The copper or copper based alloys can either be used to construct the apparatus surfaces which are susceptible to metal dusting such as reactors, or, alternatively, a coating of copper or copper based alloy can be utilized to protect an underlying surface susceptible to metal dusting.

[0021] When utilizing coatings, the copper or copper alloys can be applied to the surfaces to be protected by any technique known in the art for such an application. For example, plating, cladding, painting, chemical vapor deposition, sputtering etc.

[0022] When utilized as a coatings, the thickness of such coatings will range from about 10 to about 200 microns, preferably from about 50 to about 100 microns.

[0023] Alternatively, these compositions can be directly used as metal dusting resistant alloys. When used either as coatings or as alloys, the range of application is expressed by the following table.

METAL	TEMPERATURE °C	AMOUNT WT %
Cu-Sn	Up to about 650	About 0.1-about 2wt% Sn
Cu-Sn	Up to about 500	About 0.1 -about 5 Sn
Cu-Sn	Up to about 400	About 0.1 to about 8 wt % Sn
Cu-Ga	Up to about 650	About 0.1 to about 2 wt % Ga
Cu-Ga	Up to about 500	About 0.1 to about 5 wt% Ga
Cu-Al	Up to about 650	About 0.1 to about 4 wt% Al
Cu-Al	Up to about 500	About 0.1 to about 8 wt% Al
Cu-Sn-Ga	Up to about 650	About 0.1 to about 2wt% of Sn and Ga combined

Table (Cont'd.)

METAL	TEMPERATURE °C	AMOUNT WT %
Cu-Sn-Ga	Up to about 500	About 0.1 to about 5wt% of Sn and Ga combined
Cu-Sn-Al	Up to about 650	About 0.1 to about 2wt% Sn and about 0.1 to about 4 wt% Al
Cu-Sn-Al	Up to about 500	About 0.1 to about 5wt% Sn and about 0.1 to about 8 wt% Al
Cu-Ga-Al	Up to about 650	About 0.1 to about 2wt% Ga and about 0.1 to about 4 wt% Al
Cu-Ga-Al	Up to about 500	About 0.1 to about 5wt% Sn and about 0.1 to about 8 wt% Al
Cu-Sn-Ga-Al	Up to about 650	About 0.1 to about 2wt% of Sn and Ga combined and about 0.1 to about 4 wt% Al
Cu-Sn-Ga-Al	Up to about 500	About 0.1 to about 5wt% of Sn and Ga combined and about 0.1 to about 8 wt% Al

[0024] Surfaces susceptible to metal dusting, as described herein include those surfaces of an apparatus or reactor system that are in contact with carbon supersaturated environments at any time during use, including heat exchangers, piping, etc.

[0025] When a mixture of the above alloys is utilized, if the alloy is being exposed to a carbon supersaturated environment at temperatures up to about 500°C any combination of metals is acceptable. However, for temperatures of about 500 to about 650°C, the alloy should contain no more than about 2 wt% Sn and Ga combined.

#### EXAMPLES:

[0026] Rectangular coupons of Fe-1.25 Cr- 0.5 Mo alloy, which is considered for application as a heat exchanger material, were exposed to different CO – H<sub>2</sub> mixtures in a thermogravimetric unit at 1000°F(538°C). In

each case, the corrosion rate was measured by microscopically measuring the recession of the alloy surface with respect to an inert marker. A plot of the metal dusting rate as a function of the hydrogen content in a CO-H<sub>2</sub> gas mixture is shown in Figure 1. The metal dusting rate is seen to go through a maximum corresponding to the 50 CO: 50 H<sub>2</sub> gas mixture. Therefore, this gas mixture composition is used as the corrosive environment in all the example studies.

[0027] The resistance of Cu and Cu-Sn alloys to metal dusting corrosion at 500°C is shown in Figure 2. Since metal dusting is generally accompanied by carbon deposition, the dusting rate correlates with mass gain due to carbon deposition. While copper itself is quite resistant to metal dusting corrosion, the addition of Sn significantly improves the corrosion resistance.

[0028] The maximum temperature of application depends upon the Sn content. This is because Sn tends to vaporize at high temperatures. As shown in Figure 3, a Cu-5Sn alloy or coating can be used up to about 500°C. Above this temperature, the performance deteriorates due to Sn vaporization. For Cu-8Sn alloy, Figure 4, 400°C is an acceptable upper temperature limit.

## CLAIMS:

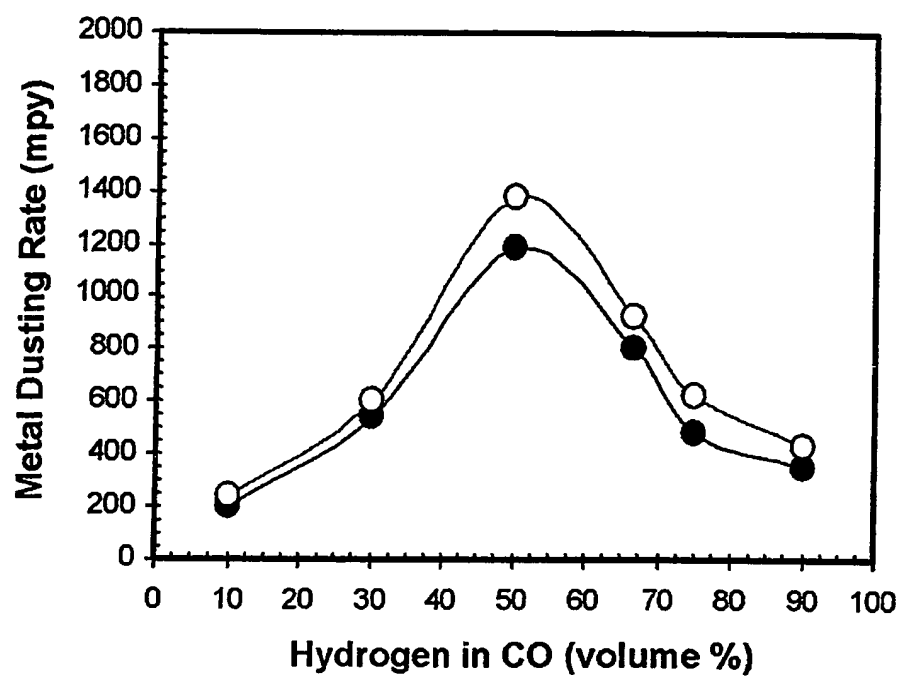
1. A composition resistant to metal dusting when exposed to a carbon super-saturated environment at temperatures up to about 650°C comprising an alloy selected from the group consisting of copper-tin alloys, copper-gallium alloys copper-aluminum alloys, and mixtures thereof, wherein when said alloy is a copper-tin alloy, the amount of tin will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures of about 400 to about 500°C, and about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 400°C, and wherein when said alloy is a copper-gallium alloy, the amount of gallium will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 up to about 650°C, and from about 0.1 to about 5 wt% for temperatures up to about 500°C, and wherein when said alloy is an copper-aluminum alloy, the amount of aluminum will range from about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and wherein when said mixture is a copper-tin-gallium alloy, the amount of tin and gallium combined will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt % when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-tin-aluminum alloy, the amount of aluminum will be about 0.1 to about 8 wt% and the amount of tin will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of aluminum will be about 0.1 to about 4 wt% and the amount of tin will

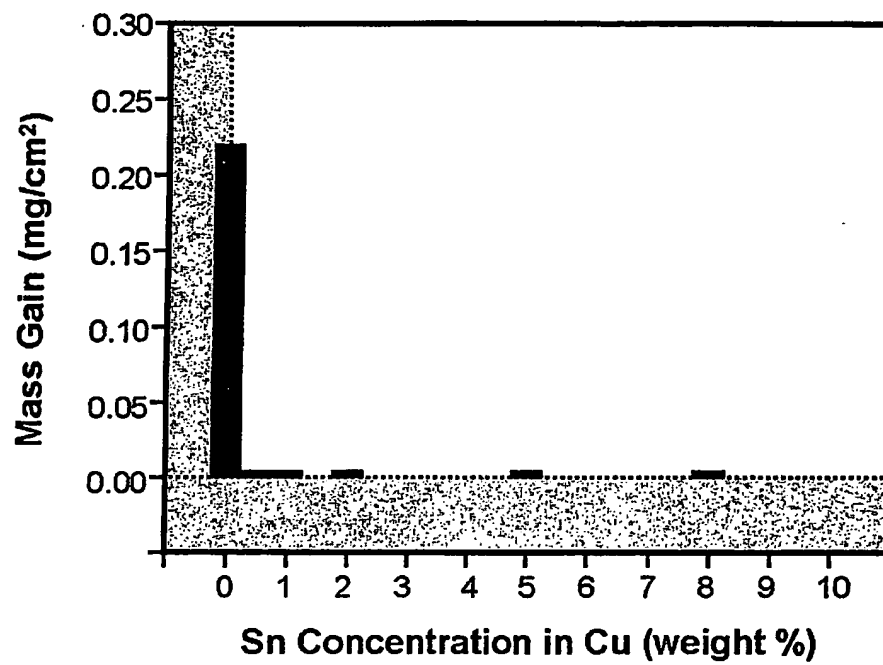
be about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-gallium-aluminum alloy the amount of gallium will be about 0.1 to about 5 wt% and the amount of aluminum will be about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of gallium will be about 0.1 to about 2 wt% and the amount of aluminum will be about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, and wherein when said mixture is a copper-tin-gallium-aluminum alloy, said alloy will contain about 0.1 to about 5 wt% of gallium and tin combined and about 0.1 to about 8 wt% aluminum when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt% of gallium and tin combined and about 0.1 to about 4 wt% aluminum when exposed to carbon supersaturated environments of between about 500 and about 650°C.

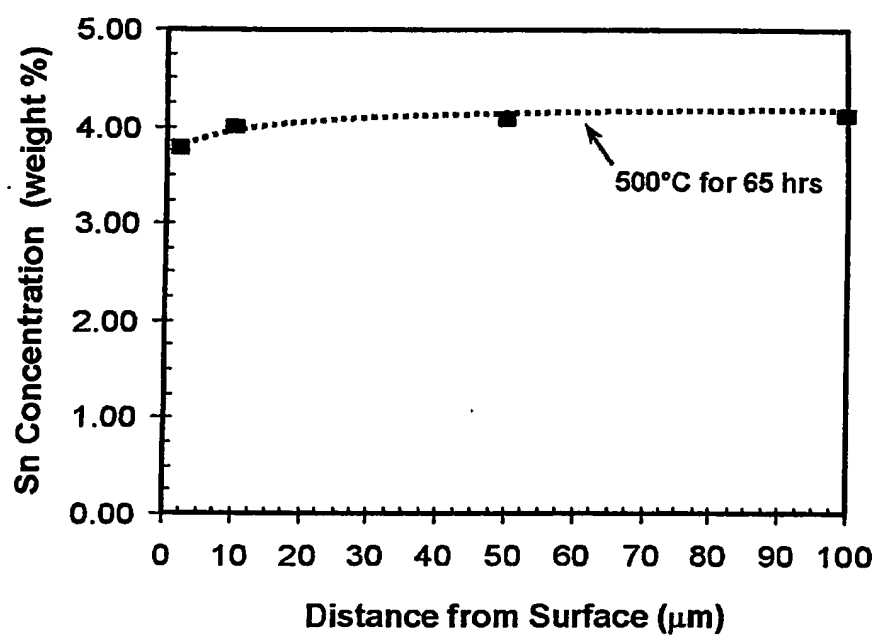
2. A method for inhibiting metal dusting of surfaces exposed to supersaturated carbon environments comprising constructing said surfaces of, or coating said surfaces with an alloy selected from the group consisting of copper-tin alloys, copper-gallium alloys copper-aluminum alloys, and mixtures thereof, wherein when said alloy is a copper-tin alloy, the amount of tin will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures of about 400 to about 500°C, and about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 400°C, and wherein when said alloy is a copper-gallium alloy, the amount of gallium will range from about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 up to about 650°C, and from about 0.1 to about 5 wt% for temperatures up to about 500°C, and wherein when said alloy is an

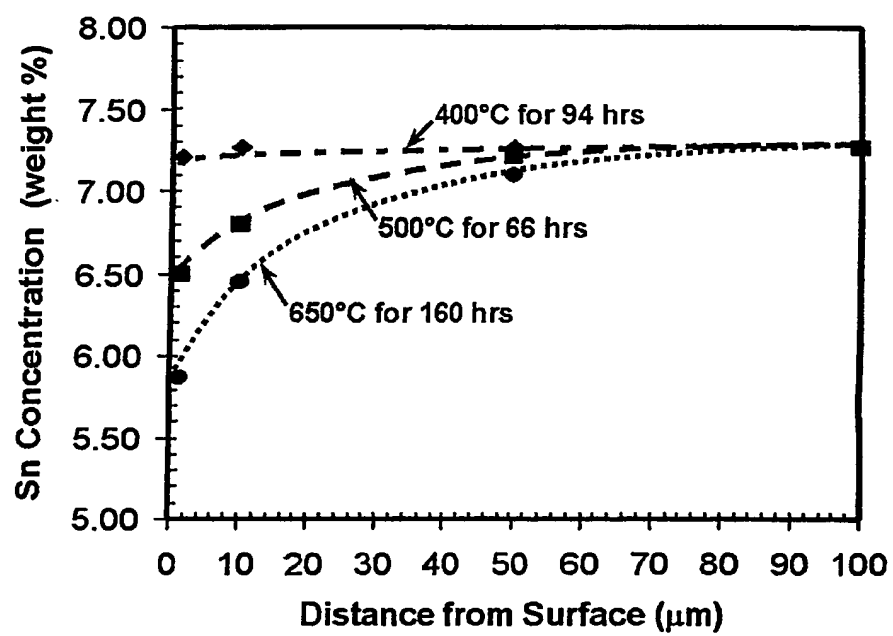
copper-aluminum alloy, the amount of aluminum will range from about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and wherein when said mixture is a copper-tin-gallium alloy, the amount of tin and gallium combined will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt % when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-tin-aluminum alloy, the amount of aluminum will be about 0.1 to about 8 wt% and the amount of tin will be about 0.1 to about 5 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of aluminum will be about 0.1 to about 4 wt% and the amount of tin will be about 0.1 to about 2 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C and wherein when said mixture is a copper-gallium-aluminum alloy the amount of gallium will be about 0.1 to about 5 wt% and the amount of aluminum will be about 0.1 to about 8 wt% when exposed to carbon supersaturated environments at temperatures up to about 500°C and the amount of gallium will be about 0.1 to about 2 wt% and the amount of aluminum will be about 0.1 to about 4 wt% when exposed to carbon supersaturated environments at temperatures of about 500 to about 650°C, and wherein when said mixture is a copper-tin-gallium-aluminum alloy, said alloy will contain about 0.1 to about 5 wt% of gallium and tin combined and about 0.1 to about 8 wt% aluminum when exposed to carbon supersaturated environments at temperatures up to about 500°C and about 0.1 to about 2 wt% of gallium and tin combined and about 0.1 to about 4 wt% aluminum when exposed to carbon supersaturated environments of between about 500 and about 650°C.

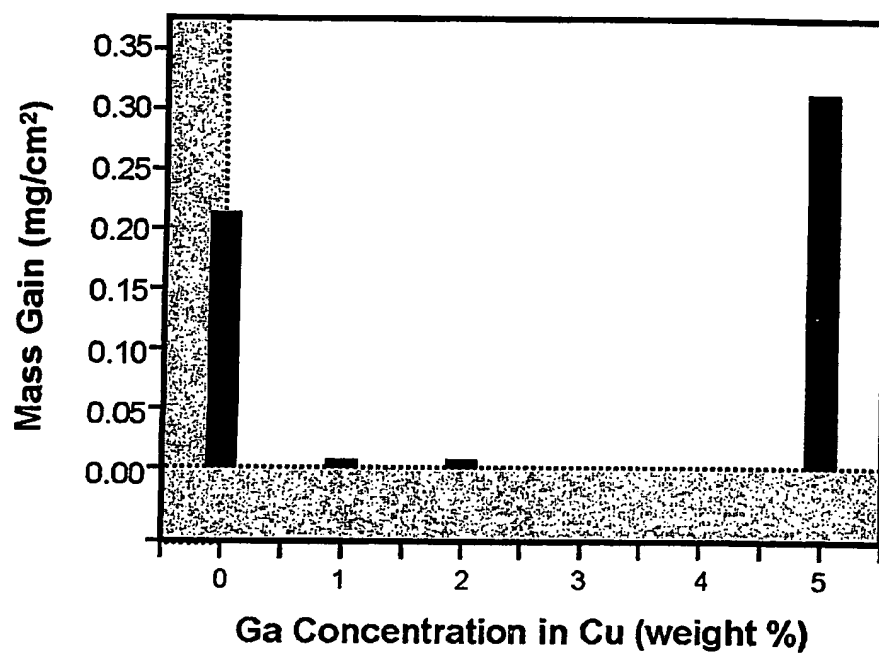
3. The method of claim 2 wherein when said surfaces are coated, said metal coating ranges from about 2 to about 100 microns in thickness.

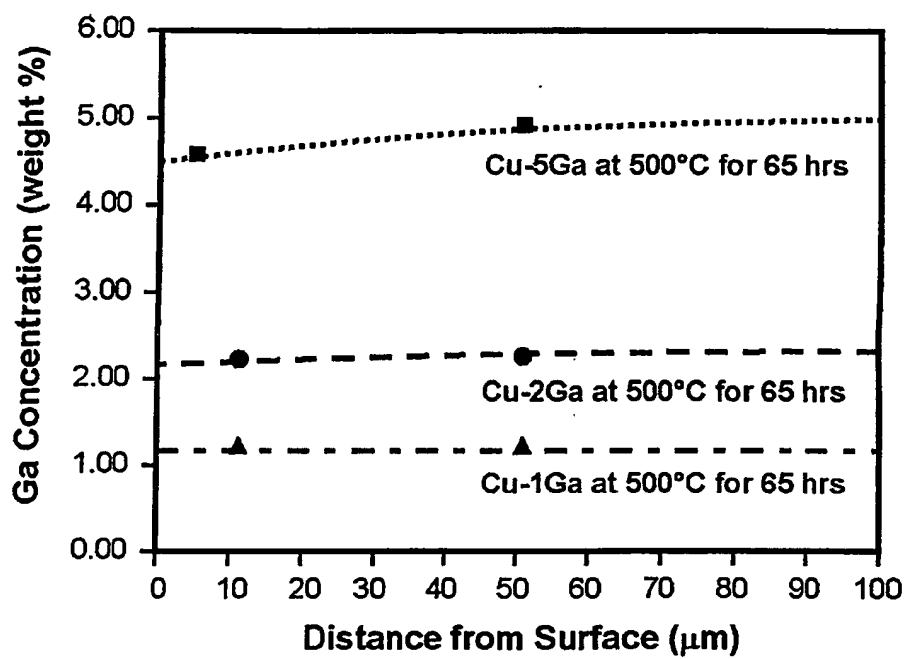
**FIG. 1**

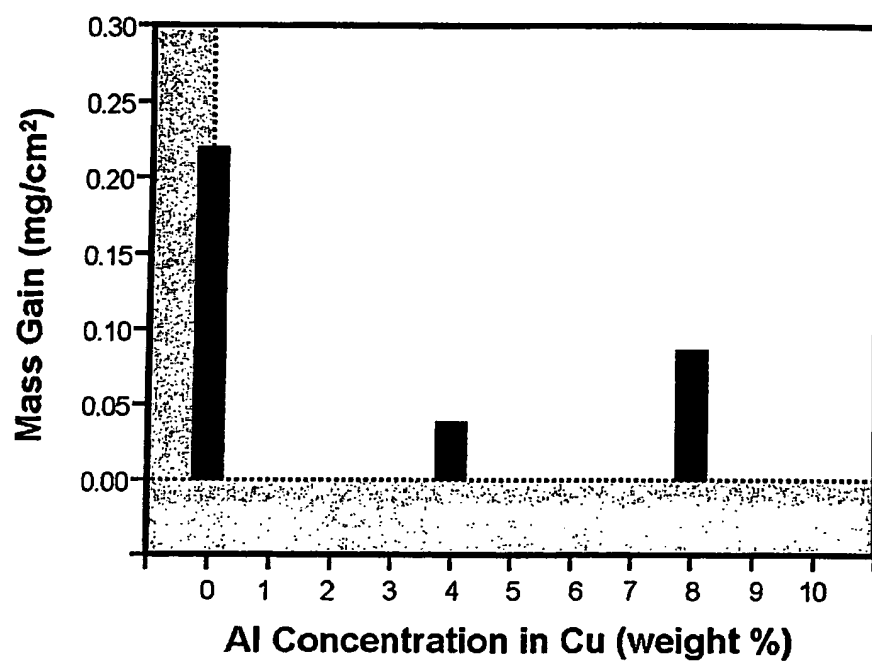
**FIG. 2**

**FIG. 3**

**FIG. 4**

**FIG. 5**

**FIG. 6**

**FIG. 7**

## INTERNATIONAL SEARCH REPORT

International Application No.

PCT/US 02/23325

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 C10G9/20 B01J19/02 C23C30/00 C22C9/00

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 C10G C23C B01J C22C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, CHEM ABS Data

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EDITOR T B MASSALSKI: "Binary Alloy Phase Diagrams volume 1" 1987, AMERICAN SOCIETY FOR METALS, OHIO/USA XP002219539 page 917	1
X	GB 448 187 A (LONDON ELECTRIC WIRE COMPANY A;MICHAEL JOHN CROWLEY) 2 June 1936 (1936-06-02) page 1, line 55 - line 61	1
X	GB 1 157 660 A (IMPERIAL METAL INDUSTRIES) 9 July 1969 (1969-07-09) page 1, line 42 - line 46	1
X	GB 1 157 658 A (IMPERIAL METAL INDUSTRIES) 9 July 1969 (1969-07-09) page 1, line 42 - line 47	1
	--- -/-	

☒ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

## \* Special categories of cited documents:

\*A\* document defining the general state of the art which is not considered to be of particular relevance

\*E\* earlier document but published on or after the international filing date

\*L\* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

\*O\* document referring to an oral disclosure, use, exhibition or other means

\*P\* document published prior to the international filing date but later than the priority date claimed

\*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

\*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

\*Y\* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

\*Z\* document member of the same patent family

Date of the actual completion of the international search

5 November 2002

Date of mailing of the international search report

15/11/2002

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
Fax: (+31-70) 340-3016

Authorized officer

Patterson, A

## INTERNATIONAL SEARCH REPORT

International Application No.

PCT/US 02/23325

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 436 790 A (PRINZ BRUNO ET AL) 13 March 1984 (1984-03-13) examples 6,7; tables	1
A	US 5 863 418 A (KUNZE ALAN G ET AL) 26 January 1999 (1999-01-26) cited in the application column 8, line 18 - line 37 column 11, line 7 - line 32	2,3
A	GB 2 066 696 A (TOYO ENGINEERING CORP) 15 July 1981 (1981-07-15) claims 1-3	2,3

## INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 02/23325

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
GB 448187	A	02-06-1936	NONE	
GB 1157660	A	09-07-1969	NONE	
GB 1157658	A	09-07-1969	NONE	
US 4436790	A	13-03-1984	DE 3116125 A1 AT 10952 T CA 1209829 A1 DE 3261673 D1 DK 179382 A EP 0065322 A1 ES 511622 D0 ES 8400495 A1 FI 821220 A ,B, JP 57181350 A NO 821238 A ,B,	25-11-1982 15-01-1985 19-08-1986 07-02-1985 24-10-1982 24-11-1982 16-10-1983 16-01-1984 24-10-1982 08-11-1982 25-10-1982
US 5863418	A	26-01-1999	US 5674376 A US 5676821 A AT 159040 T AU 665534 B2 AU 1580192 A BR 9205738 A CA 2105305 A1 CN 1067258 A ,B DE 69222633 D1 DE 69222633 T2 EP 0576571 A1 EP 0798363 A2 EP 0845521 A1 ES 2108112 T3 HU 75107 A2 JP 6507191 T JP 2001220586 A KR 230727 B1 OA 9910 A SG 72690 A1 WO 9215653 A1 FI 933880 A	07-10-1997 14-10-1997 15-10-1997 11-01-1996 06-10-1992 23-08-1994 09-09-1992 23-12-1992 13-11-1997 23-04-1998 05-01-1994 01-10-1997 03-06-1998 16-12-1997 28-04-1997 11-08-1994 14-08-2001 15-11-1999 15-09-1994 23-05-2000 17-09-1992 01-10-1993
GB 2066696	A	15-07-1981	JP 56084789 A AU 6536780 A BR 8008164 A CA 1140162 A1 CS 226024 B2 DD 155140 A5 DE 3046412 A1 FR 2472035 A1 IN 153575 A1 PL 228425 A1	10-07-1981 18-06-1981 30-06-1981 25-01-1983 19-03-1984 19-05-1982 10-09-1981 26-06-1981 28-07-1984 07-08-1981